

### Effects of Turbulence on Hydraulic Heads and Parameter Sensitivities in Preferential Ground-Water Flow Layers



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#### Project Funded by USGS Ground-Water Resources Program Kevin Dennehy, Program Manager



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### WHAT IS TURBULENT GROUND-WATER FLOW ?



### Fluid Inertial Forces > Viscous Forces



Streamlines trace out the path of a 'mass-less' particle moving within the ground-water flow system.



### WHAT IS TURBULENT GROUND-WATER FLOW ?

Reynolds numbers indicate whether flow is laminar or turbulent

$$R_e = \frac{\rho q d}{\mu} = \frac{inertial \ forces}{viscous \ forces}$$

# Flow is turbulent when the critical Reynolds number $(N_{Re})$ is exceeded

$$R_e > N_{\text{Re}}$$
, flow is turbulent

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### WHAT IS TURBULENT GROUND-WATER FLOW ?



Notice turbulence decreases Specific Discharge, energy is lost to eddies

#### Darcy's Law is not valid for turbulent flow

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### WHY STUDY TURBULENT FLOW ?

It's fundamental hydrology





 Could explain most groundwater movement in karst

- Implications for:
  - Fate of injected waters
    - ASR
    - Wastewater
  - Saltwater intrusion
  - Nutrient loading (from submarine groundwater discharge)
  - Contaminate transport



Streamlines trace out the path of a 'mass-less' particle moving within the ground-water flow system.



### **Conduit Flow Process Mode 2 (CFPM2)**



A product of the Ground-Water Resources Program

### Documentation of a Conduit Flow Process (CFP) for MODFLOW-2005



Techniques and Methods, Book 6, Chapter A24

U.S. Department of the Interior U.S. Geological Survey



### **CFPM2 Governing Flow Equation**

Traditional MODFLOW with Darcy's Law and laminar hydraulic conductivity

$$\frac{\partial}{\partial x} \left( \frac{Klam_{xx}}{\partial x} \frac{\partial h}{\partial x} \right) + \frac{\partial}{\partial y} \left( \frac{Klam_{yy}}{\partial y} \frac{\partial h}{\partial y} \right) + \frac{\partial}{\partial z} \left( Klam_{zz} \frac{\partial h}{\partial z} \right) + W = S_s \frac{\partial h}{\partial t}$$

CFP Mode 2 computes horizontal turbulent flow using turbulent hydraulic conductivity.

$$\frac{\partial}{\partial x} \left( Kturb_{xx} \frac{\partial h}{\partial x} \right) + \frac{\partial}{\partial y} \left( Kturb_{yy} \frac{\partial h}{\partial y} \right) + \frac{\partial}{\partial z} \left( Klam_{zz} \frac{\partial h}{\partial z} \right) + W = S_s \frac{\partial h}{\partial t}$$



### **CFPM2 Turbulent K**

Turbulent horizontal hydraulic conductivity ( $K_{turb}$ ) is a non-linear function of the Reynolds Number (Re) after critical Reynolds number ( $N_{Re}$ ) is exceeded.

$$K_{turb} = F_{adj}K_{lam}$$

$$F_{adj_{kiter}} = \sqrt{\frac{K_{lam} \Delta h_{crit}}{K_{turb_{kiter-1}} \Delta h_{kiter-1}}}$$

Derived by Kuniansky and Halford, 2008

$$\Delta h_{crit} = \frac{N_{\rm Re} \Delta l v}{K_{lam} d_{pore}}$$



### **CFPM2 Benchmark Testing**





### **CFPM2** Testing



Permeameter Data Verify New Turbulence Process for MODFLOW By Eve L. Kuniansky and others.











**Picture from Kevin Cunningham, USGS** 





Hydrogeologic conceptualization of Lake Belt area from: Cunningham and Dixon, written communication



To estimate  $K_{lam}$ , one could use the resistance terms in the Darcy-Weisbach equation, limited by effective porosity. Limiting by effective porosity accounts for the resistance offered by "dead end" voids.

$$K_{lam} = \left(\frac{gd^2}{32\nu}\right)\theta$$

Derived by Eve Kuniansky, 2008



# Table 1. Initial estimates of laminar horizontal hydraulicconductivity for preferential flow layers

Layer	Source Data	Number Wells	Mean Effective Porosity (%)	Number of Measurement On cores or images	Mean Vug Diameter (CM)	Laminar Horizontal Hydraulic Conductivity (meters per day)
2	Direct Measurement on cores	23	11.8	240	0.9	200,000
5	Direct Measurement on cores	6	18.3	65	0.8	300,000
8	Mostly Measurements from digital borehole wall images	22	14.8	438	3.5	5,000,000

Data from Kevin Cunningham and others, 2006



Table 3. Cri Model Scenar	itical Reynolds	Numbers	Assigned	for	Turbu lent
Scenario					$N_{Re}$
S1					11
S2					55
S3					440
S4					11 00
S5					2200

#### **Critical reynolds numbers are uncertain**



**Upper critical** Reynolds Number equals 55







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#### **CFPM2 APPLICATION TO BISCAYNE AQUIFER**





## Summary

1. Extent of turbulent flow increases with increasing hydraulic conductivity, mean void diameter, groundwater temperature, and decreasing critical Reynolds numbers.

2. When turbulence was active (occurring in about 56% of preferential flow model cells), head differences from laminar elevations ranged from about 18 to +27 cm.

3. The composite-scaled sensitivities of horizontal hydraulic conductivities decreased by as much as 70% when turbulence was essentially removed.

4. This study highlights potential errors in model calculations based on the equivalent porous media assumption, which assumes laminar flow in uniformly distributed void spaces



## Limitations

- Macro-scale <u>simplification</u> of impacts of turbulent flow
- Vast uncertainty in aquifer hydraulic properties
  and boundaries
- Theory is sound, but applications on systems with uncertainty may produce unreliable predictions

### Thanks ! For more information, bshoemak@usgs.gov

Shoemaker, W. B., K. J. Cunningham, E. L. Kuniansky, and J. Dixon (2008), Effects of turbulence on hydraulic heads and parameter sensitivities in preferential groundwater flow layers, Water Resour. Res., 44, W03501, doi:10.1029/2007WR006601.

Picture taken by Eve Kuniansky of field trip to Fish River Cave near Yangshuo, China,